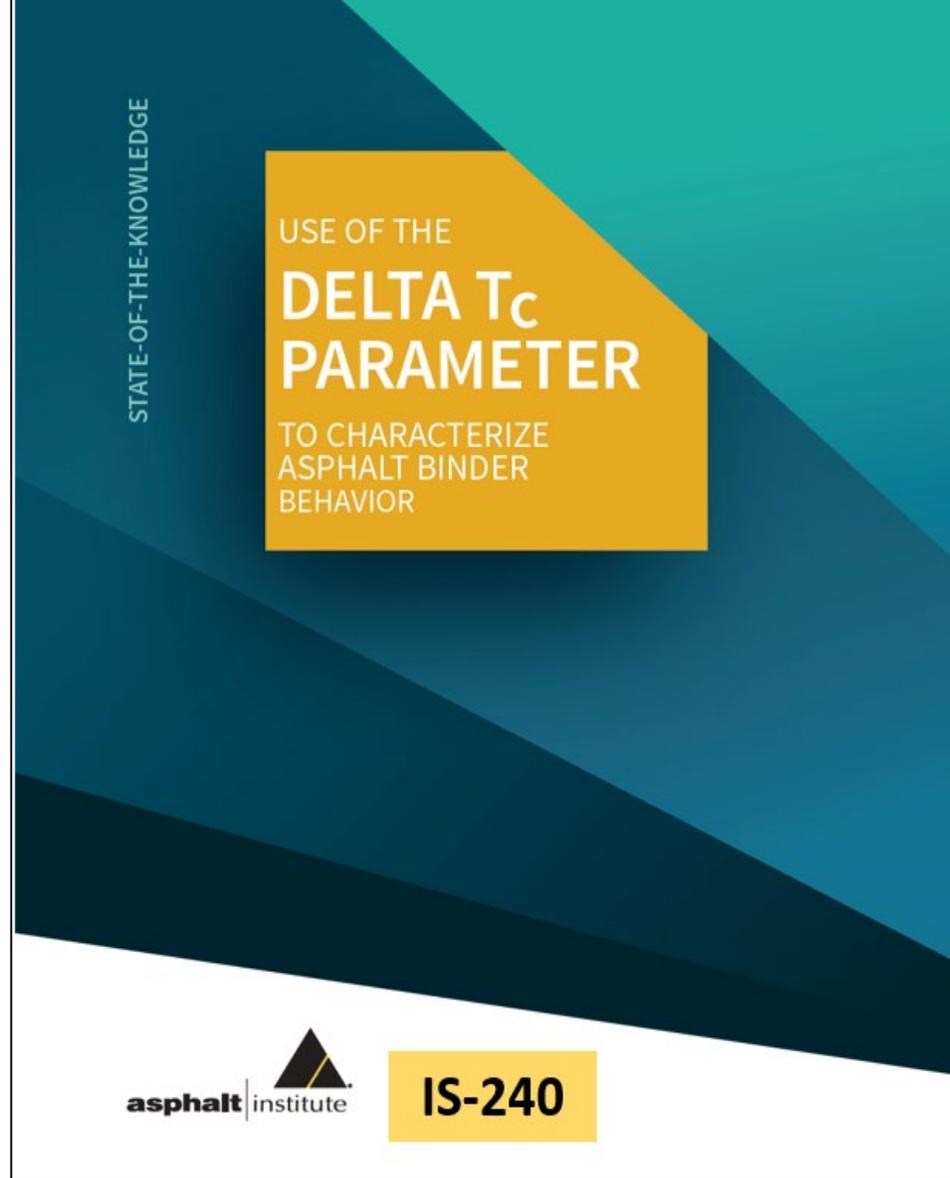


# State-of-the-Knowledge Document on Delta $T_c$

53<sup>rd</sup> Mid-Atlantic QAW  
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- 11 chapters, 64 pages
- Free download as e-Book on AI's website (under Engineering)



## TABLE OF CONTENTS

<b>1.0 Introduction and Purpose</b> .....	4
<b>2.0 Origin of <math>\Delta T_c</math></b> .....	5
Comments on Originating Study: AATP Project 06-01 .....	10
<b>3.0 The Mechanics of <math>\Delta T_c</math></b> .....	11
Calculation of $\Delta T_c$ .....	11
What the $\Delta T_c$ Number Means.....	12
What $\Delta T_c$ Looks Like.....	15
<b>4.0 What Affects <math>\Delta T_c</math>?</b> .....	19
Laboratory Aging.....	19
Reclaimed Asphalt Pavement (RAP) .....	27
Recycled Asphalt Shingles (RAS) .....	29
Re-refined Engine Oil Bottoms (REOB) .....	32
Combined Effects .....	35
Elastomeric Polymer Modification.....	38
Other Asphalt Characteristics .....	42
<b>5.0 Considerations When Using <math>\Delta T_c</math></b> .....	45
Distress Types that $\Delta T_c$ Addresses .....	45
Recovered Binder in Relation to $\Delta T_c$ .....	46
Precision .....	46
Practical Considerations.....	46
<b>6.0 Full-Scale Test Projects and <math>\Delta T_c</math></b> .....	48
<b>7.0 Perceived Utility of <math>\Delta T_c</math></b> .....	51
Asphalt Institute Survey .....	51
Agency Specifications .....	52
Considerations for Implementation of $\Delta T_c$ as a Specification Parameter .....	55
Alternatives to $\Delta T_c$ for Addressing Block Cracking.....	56
<b>8.0 Recent National Research Projects and <math>\Delta T_c</math></b> .....	57
<b>9.0 Summary</b> .....	58
<b>10.0 References</b> .....	60
<b>11.0 Frequently Asked Questions</b> .....	63

<http://www.asphaltinstitute.org/engineering/delta-tc-technical-document/>

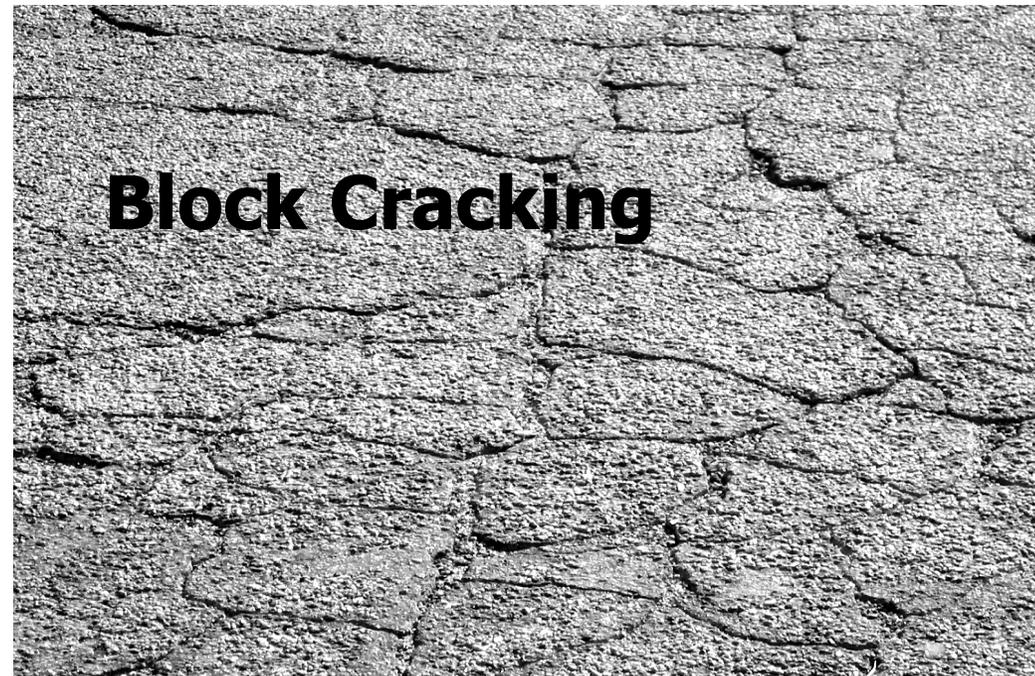
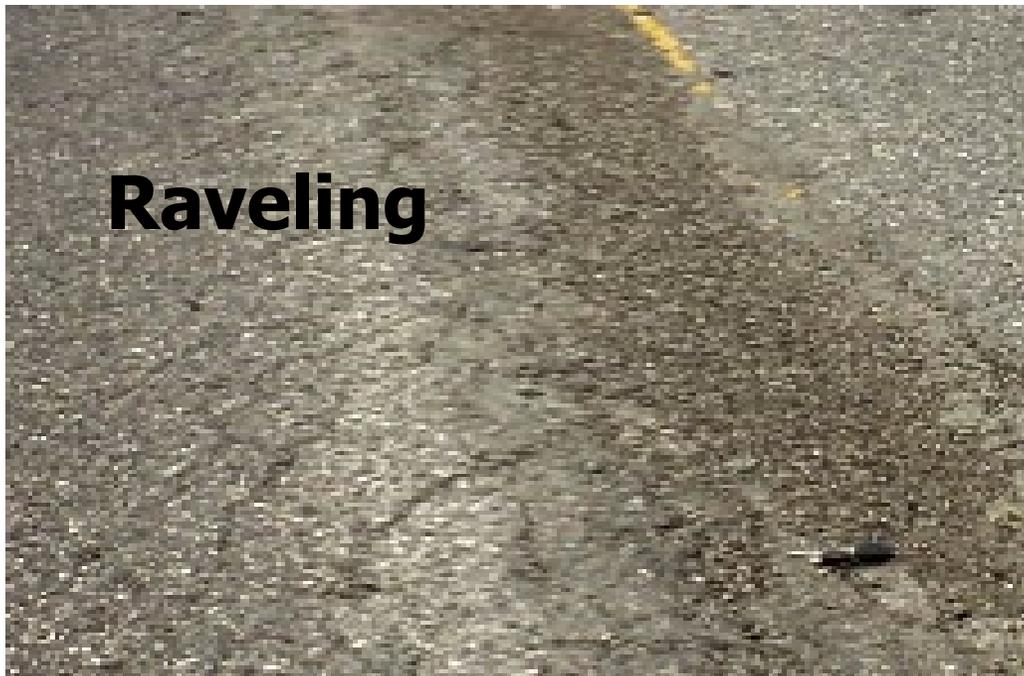
- IS document is a technical “state of the knowledge” document that captures the consensus of the asphalt binder suppliers in the United States on a wide variety of topics related to:
  - Aging/testing
  - Pass/Fail criteria
  - Adoption of  $\Delta T_c$  in a binder purchase specification
- Not intended to provide guidance
- Asphalt Institute does not take a position on the adoption of  $\Delta T_c$  in a binder purchase specification

- AI TAC decided in April 2019 to develop this document
- Why
  - More and more agencies looking to implement  $\Delta T_c$  in binder purchase spec
  - Relevant info on  $\Delta T_c$  was scattered
  - Difficult to sort through relevant sources
- Need
  - Single, comprehensive, up-to-date reference
  - Focal point for dialog to those wanting a better understanding of  $\Delta T_c$  and its relevance in characterizing binder behavior

# Delta Tc Background

# What is $\Delta T_c$ ?

- Asphalt durability parameter derived from low temp BBR test and results (S and m)
- Provides insight into binder relaxation properties that contribute to non-load related cracking and other age-related embrittlement distresses



# What is $\Delta T_c$ ?



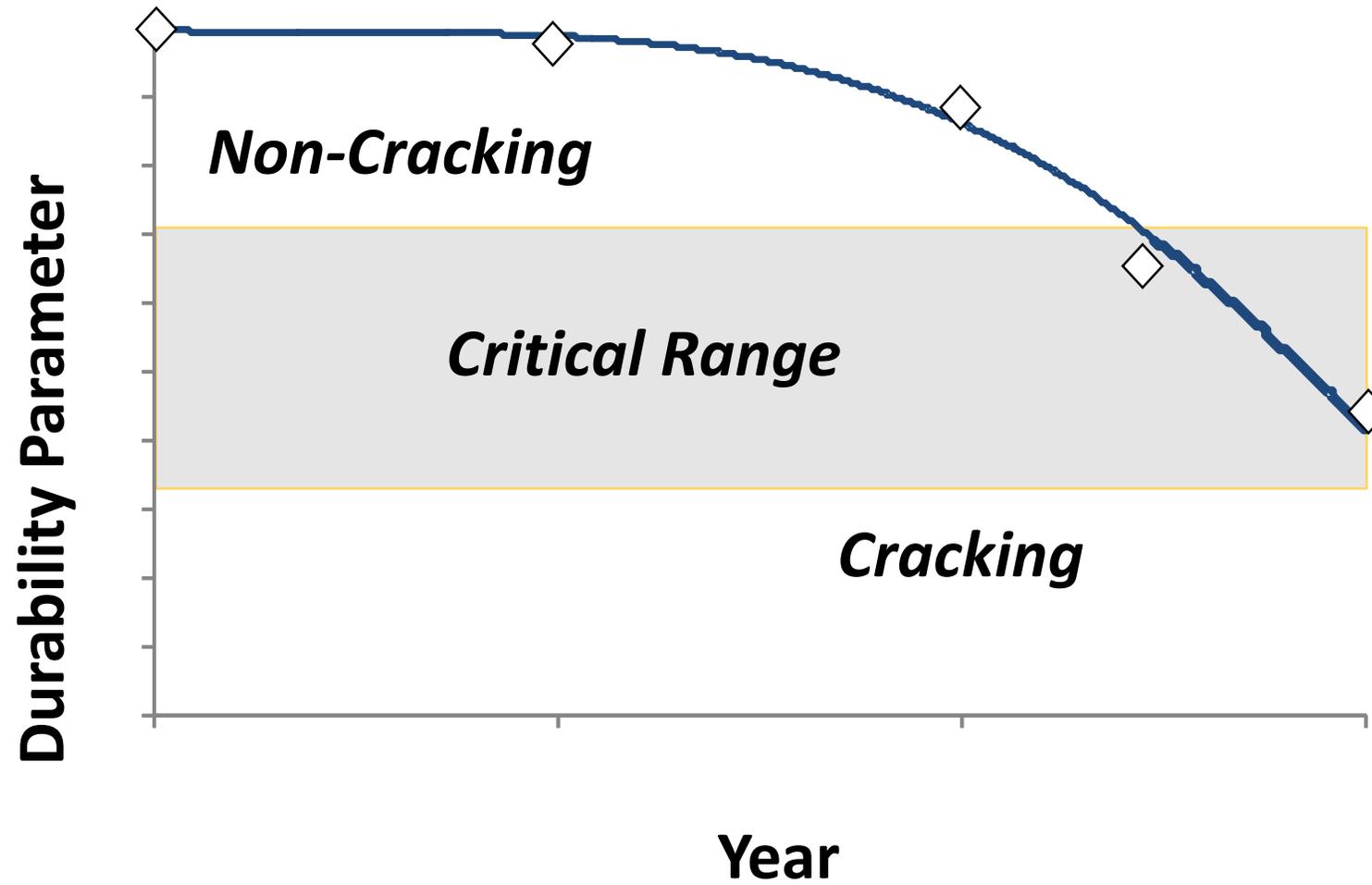
- Conceptualized by Anderson, et al. in Journal AAPT, Vol. 80, 2011
  - FAA sponsored study, AAPT 06-01 Techniques for Prevention and Remediation of Non-Load-Related Distresses on HMA Airport Pavements
  - Intended as a forensic analysis of existing airfield pavements
  - Aimed at timing of preventive maintenance
- Since 2011 gained interest as specification parameter by DOT's

- Objectives

- Develop a practical guide identifying means to prevent and mitigate cracking caused by environmental effects.
- Develop one or more test procedures that could be used by a pavement manager to determine when preventative maintenance is needed to prevent the development of cracking (specifically block cracking).



- TPF-5(153) Optimal Timing of Preventive Maintenance for Addressing Environmental Aging in Hot-Mix Asphalt Pavements
  - MN, MD, OH, TX, WI, LRRB
- Primary Objective
  - to develop and validate technology that can be used by highway agencies to determine the proper timing of preventive maintenance in order to mitigate damage caused by asphalt aging

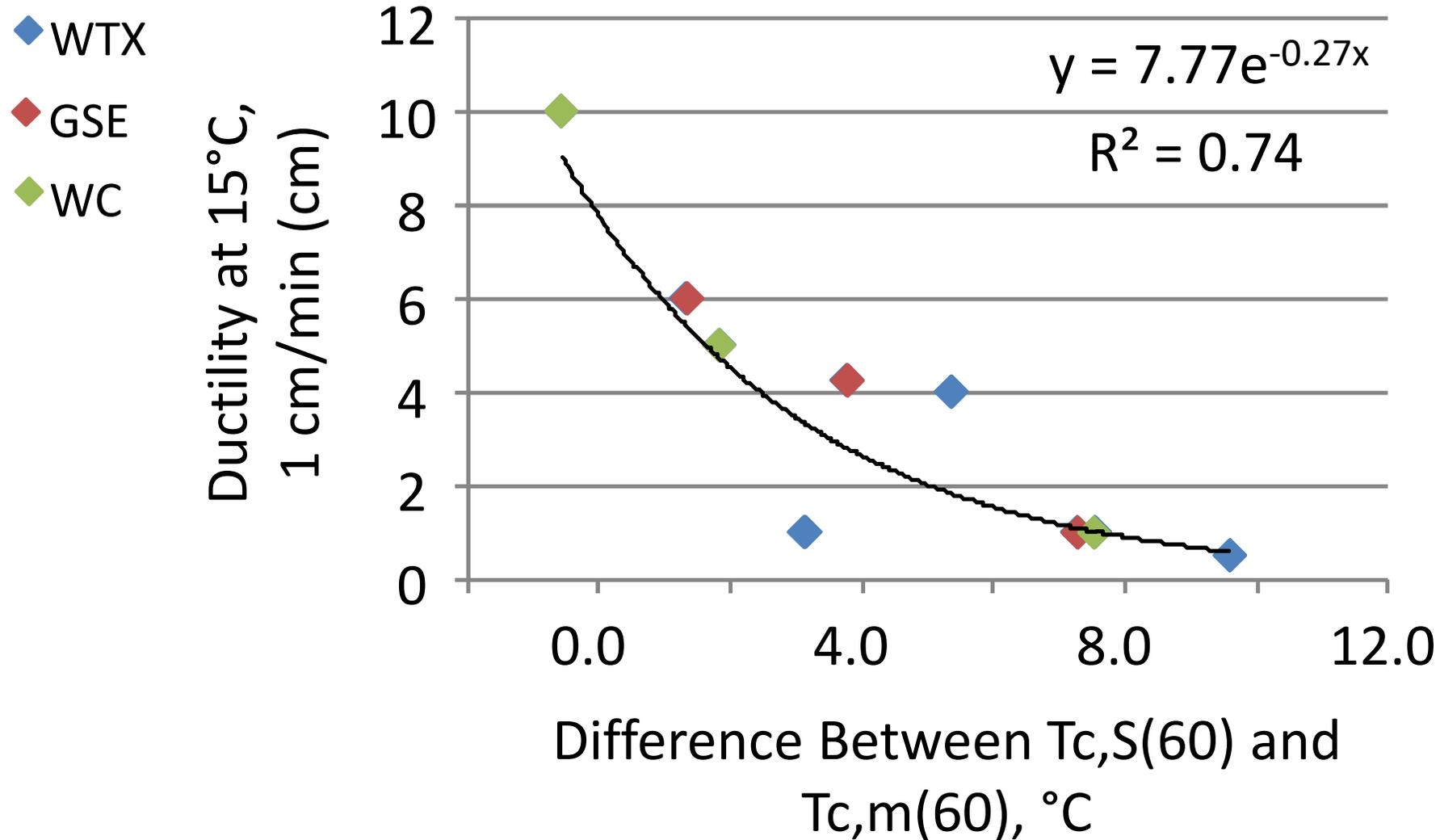


- In-service aging leads to oxidation and loss of flexibility at intermediate and low temperatures
  - Block-cracking
    - when environmental (non-load) conditions create thermal stresses that cause strain in the asphalt mixture that exceeds the failure strain

- In-service aging leads to oxidation and loss of flexibility at intermediate and low temperatures
  - Preventing or mitigating distress
    - identify a property of the asphalt binder or mixture that sufficiently correlates with its flexibility
    - provide a procedure to monitor when flexibility reaches a state where corrective action is needed

- Physical Changes – Ductility
  - Block cracking severity related to ductility at 60°F (15°C) – Kandhal (1977)
    - “Low-Temperature Ductility in Relation to Pavement Performance”, ASTM STP 628, 1977
  - Loss of surface fines as ductility = 10 cm
  - Surface cracking when ductility = 5 cm
  - Serious surface cracking when ductility < 3 cm

# Relationship between $\Delta T_c$ and Ductility



Delta Tc

What is it and How is it Determined?

# What is Delta Tc ( $\Delta T_c$ )

- **Delta Tc ( $\Delta T_c$ )** is a parameter that provides insight into the relaxation properties of an asphalt binder which can contribute to non-load related cracking or other age-related embrittlement distresses in an asphalt pavement.
- It is a calculated value using the results (S and m) from the BBR test.
- It is intended to be used on binder that has been short and long-term aged (RTFO plus PAV)
- Can also be used on binder recovered from asphalt pavements

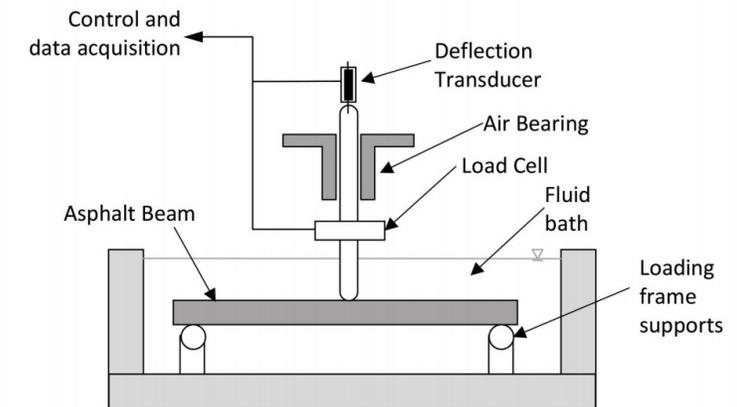
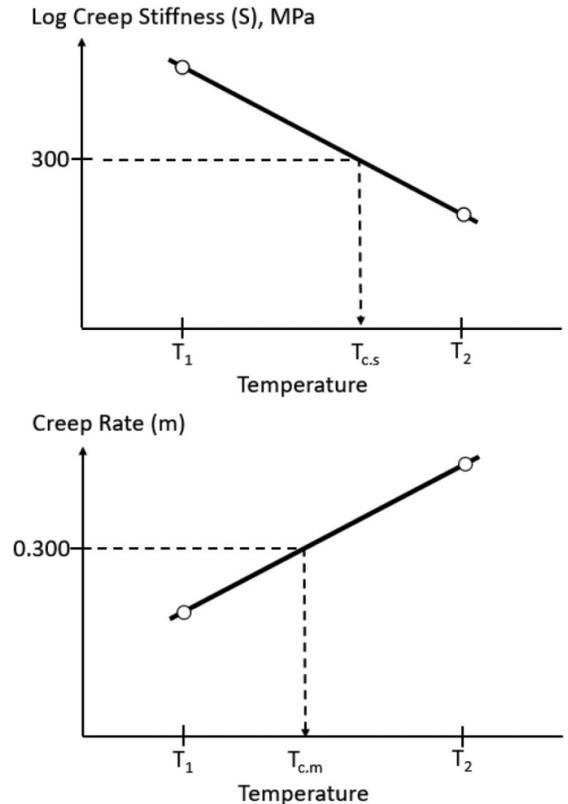


Figure 8. Simple Schematic of BBR Test Apparatus

# What is Delta Tc ( $\Delta T_c$ )?

- Delta Tc ( $\Delta T_c$ ) is the difference between the critical low temperatures of the asphalt binder, determined using the Bending Beam Rheometer (BBR), where the stiffness (S) at 60 seconds of loading time is exactly equal to the specification value of 300 MPa and the m-value (m) at 60 seconds of loading time is exactly equal to the specification value of 0.300.



# What Does $\Delta T_c$ Represent?

- $\Delta T_c$  represents the relationship between stiffness and relaxation
  - As aging occurs,  $S$  increases and  $m$  decreases
  - Similar response at intermediate temperatures for  $G^*$  (increases) and  $\delta$  (decreases)
  - Balance between change in stiffness and proportion of viscous and elastic properties

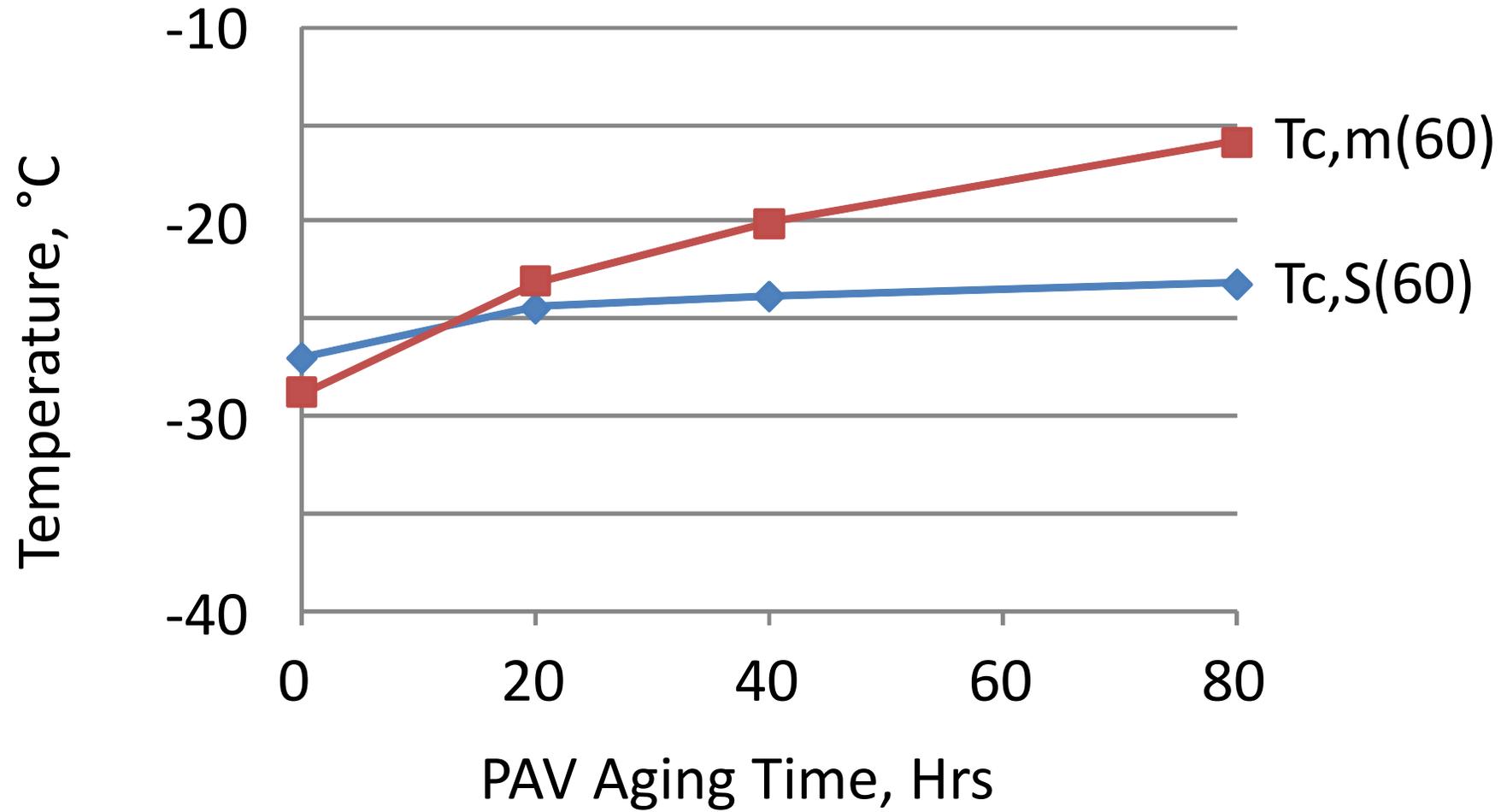
- Calculate the value of  $\Delta T_c$  :

$$\Delta T_c = T_{c,S} - T_{c,m}$$

- Positive values of  $\Delta T_c$  indicate an S-controlled asphalt binder
- Negative values of  $\Delta T_c$  indicate an m-controlled asphalt binder

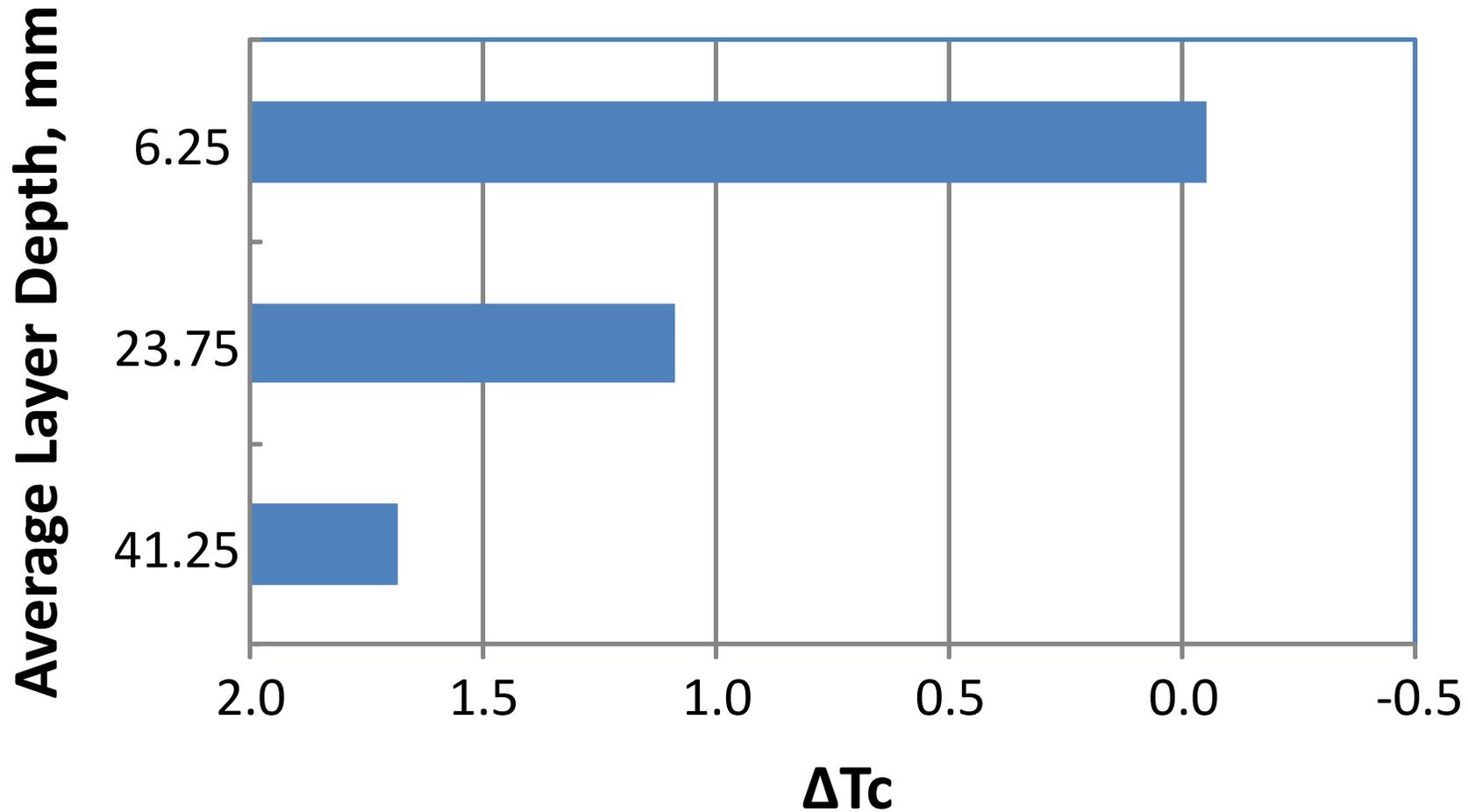
- **$\Delta T_c$  is related to the relaxation properties of a binder. What is relaxation and how does binder relaxation properties relate to mixture performance?**
  - Asphalt exhibits a bit of viscous behavior, even at low temperatures when its behavior is mostly considered elastic.
  - Therefore, when thermal stresses build up as a pavement gets colder, the asphalt binder will gradually experience viscous flow and the stresses will greatly reduce.
    - This reduction of stresses over time is what is known as relaxation.
    - In general, as a binder ages, its relaxation properties are diminished.
    - An asphalt pavement that has a binder with good relaxation properties will be less likely to have durability-related cracking than a pavement containing a binder with poor relaxation properties.

# BBR: Gulf-Southeast (GSE)

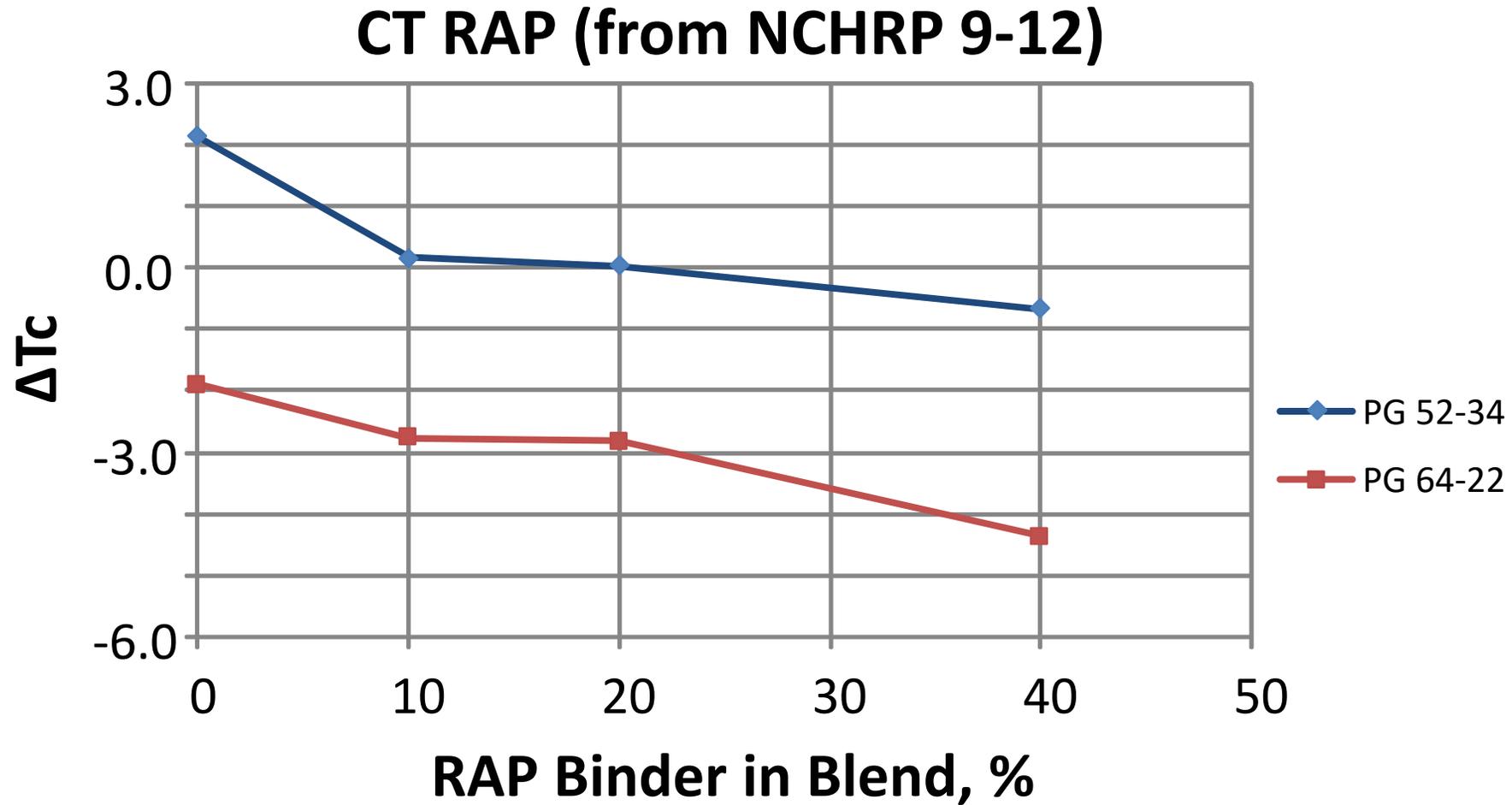


# $\Delta T_c$ is an Indicator of Oxidative Aging

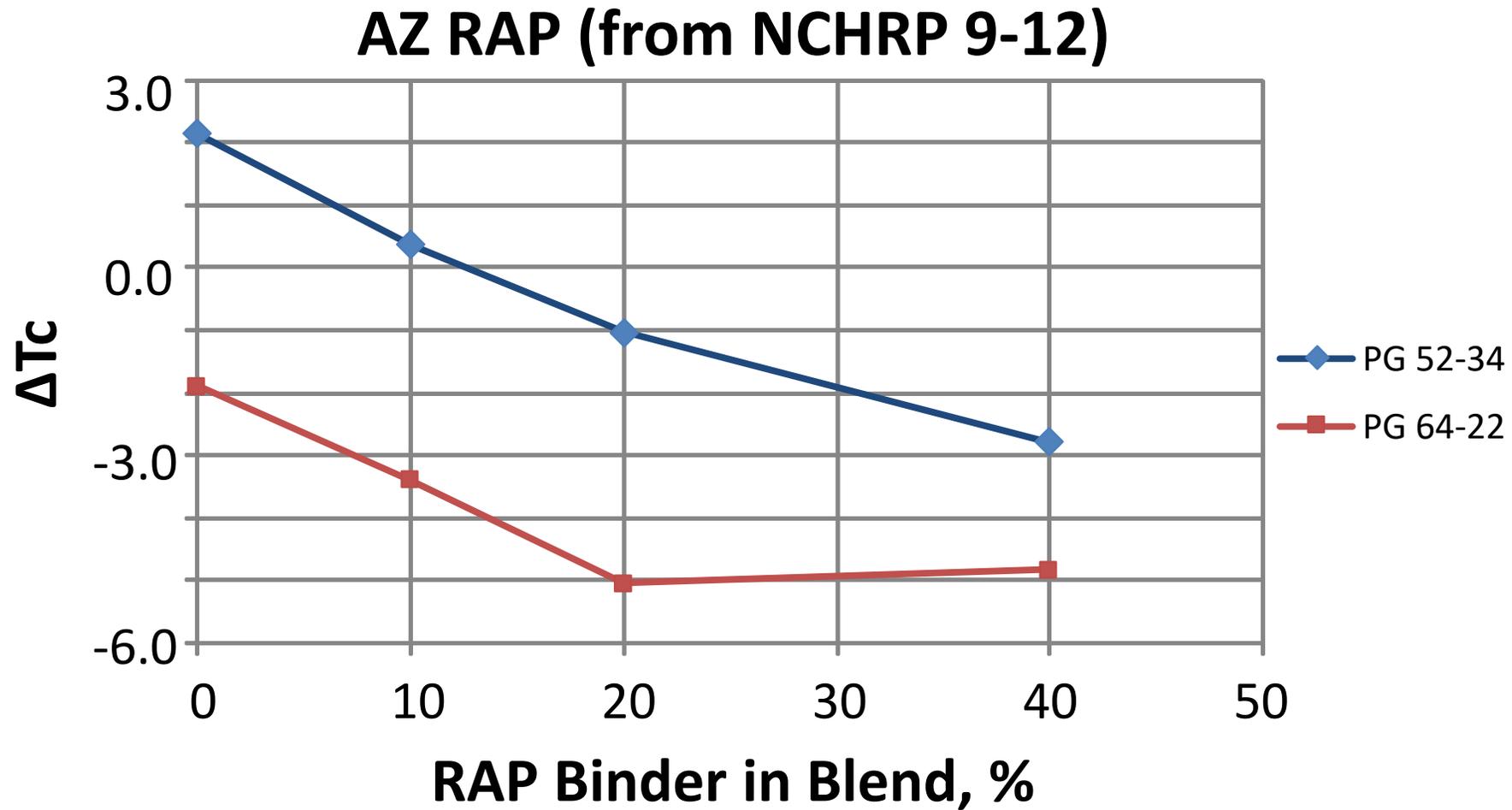
## MnROAD Cell 24



# $\Delta T_c$ is an Indicator of Oxidative Aging



# $\Delta T_c$ is an Indicator of Oxidative Aging



# Can $\Delta T_c$ be used to predict cracking?

- $\Delta T_c$  is thought to be **directly** related to block cracking.
  - However, fatigue, edge, longitudinal, reflection, and transverse cracking may indirectly be related to  $\Delta T_c$  of the binder.
    - These distress types are typically caused by other factors, yet  $\Delta T_c$  can play a supporting role in their development.



- BBR Limitations

- Often cannot interpolate  $T_{c,m}$  for highly negative values of  $\Delta T_c$ 
  - Stiffness is too low at temperatures where m-value approaches 0.300
  - Concerns about excess deflection
  - RAP/RAS
- Polymer Modified Asphalt Binders
  - Have a higher elastic component at a given stiffness due to the polymer
  - Result is lower (more negative) values of  $\Delta T_c$

- **What are some things that an agency should consider before implementing  $\Delta T_c$  in a purchase specification?**
  - A brief summary of these steps is described in the “Considerations for Implementation of  $\Delta T_c$  as a Specification Parameter” section of the document
  - When implementing important specification changes, AI encourages agencies to work together regionally (such as in User-Producer Groups) to facilitate uniform transition for the asphalt industry.

# Step #1: Identify issues to be solved

- **Clearly identify the pavement performance challenge that  $\Delta T_c$  is intended to solve**
  - Without this clear statement of purpose, it is possible that a specification change will not mitigate the intended problem.
  - $\Delta T_c$  is primarily aimed at asphalt pavement distress that is related to a lack of durability exhibited by asphalt binders. The most prominent distress that  $\Delta T_c$  targets is block cracking of aged asphalt pavements, which was the damage for which  $\Delta T_c$  was originally developed to predict.

# Step #2: Is $\Delta T_c$ is the best parameter?

- **Determine whether  $\Delta T_c$  is the best parameter to solve the problem identified in the first step**
  - Determination of  $\Delta T_c$  potentially has an onerous effect on laboratory workflow.



# Step #3: Determine amount of aging needed

- **Consider what form of laboratory aging needs to be used to simulate pavement aging so that  $\Delta T_c$  measurements are made on representative samples**
  - This step, along with Step #4, ensures that the  $\Delta T_c$  specification is relevant
  - To accomplish this, a variety of PG binders should be laboratory aged, typically using variations on AASHTO R28
  - At present, 20- and 40-hours of pressure aging are most commonly used for  $\Delta T_c$  determinations

# Step #4: Sample existing asphalt pavement

- **Sample existing asphalt pavements, preferably in service for at least five years, and measure  $\Delta T_c$  on in-situ materials**
  - Asphalt pavements exhibiting poor performance clearly due to asphalt durability as well as good-performing pavements should be sampled in the form of cores
  - Because aging occurs most rapidly in the materials most exposed to the elements, asphalt binder from the top ½-inch (12.5 mm) of the core should be extracted and recovered for determination of  $\Delta T_c$ 
    - This is considered a conservative approach in determining  $\Delta T_c$  because it represents a worst case for aging

- **Sample existing asphalt pavements, preferably in service for at least five years, and measure  $\Delta T_c$  on in-situ materials (continued)**
  - However, if in the first step it is decided that  $\Delta T_c$  needs to target the asphalt binder contribution to load-associated damage, it might be desirable to evaluate  $\Delta T_c$  for lower asphalt layers
  - When extracting/recovering asphalt materials, consideration should be given to using toluene as it is accepted as a standard solvent that is well-suited for the evaluation of polymer-modified asphalt binders

# Step #5: Determine aging protocol

- **Evaluate the  $\Delta T_c$  test results obtained in the previous step to arrive at the aging protocol necessary to simulate the  $\Delta T_c$  values obtained in service**
  - Laboratory aging data from step three (laboratory aging required to simulate in-service pavement aging) be employed for this purpose.
  - The last step is to conduct a discriminate analysis to arrive at  $\Delta T_c$  value that distinguishes between good and poor pavement performance

# Step #6: Evaluate data to determine $\Delta T_c$ criteria

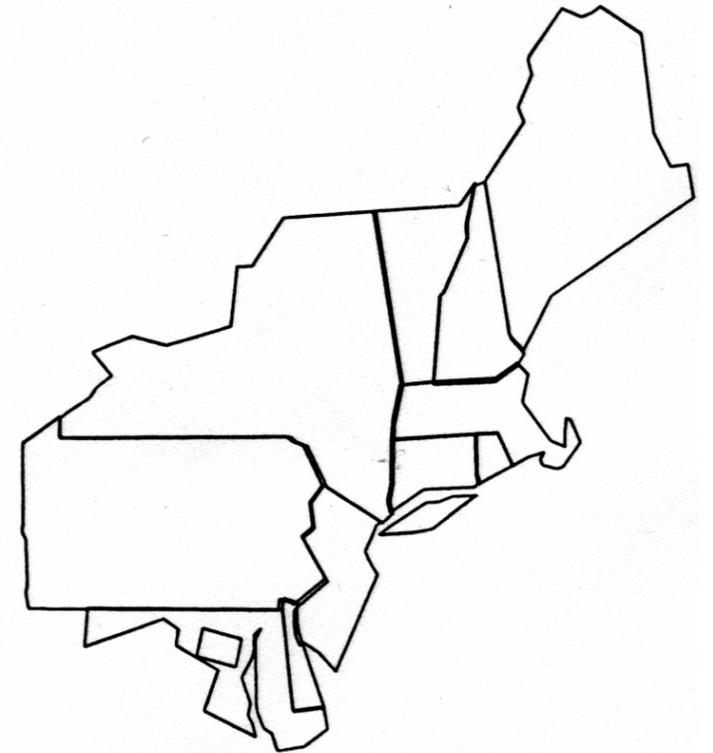
- Conduct a discriminant analysis to arrive at a  $\Delta T_c$  value that distinguishes between good and poor pavement performance with respect to age-related embrittlement or other distress type under consideration





# How variable is $\Delta T_c$ (NEAUPG Study) ?

- Phase 2 - 23 labs ( 11 suppliers, 9 DOT's, FHWA, 2 Universities)
- One engineered binder
  - Binder A – PG 64S-22
- Four Aging Conditions:
  - Method A – Standard 20-hour PAV
  - Method B – 20+20-hour PAV
  - Method C – 20+4+20-hour PAV
  - Method D – 40-hour PAV
  - **Method E – Standard 20-hour PAV w/12.5 grams per pan**



# How variable is $\Delta T_c$ ?

**Table 2. Northeast Asphalt User Producer Group Extended Laboratory Aging Study (7)**

BBR Property	PG 58S-28				
	Method A	Method B	Method C	Method D	Method E
Avg m-value @ -18°C	0.322	0.286	0.285	0.285	-
Avg stiffness @ -18°C	243	283	280	278	-
Avg m-value @ -24°C	0.261	0.242	0.235	0.241	-
Avg stiffness @ -24°C	494	530	531	541	-
Avg $\Delta T_c$ , °C	+0.3	-3.2	-2.6	-2.6	-

BBR Property	PG 64E-22				
	Method A	Method B	Method C	Method D	Method E
Avg m-value @ -12°C	0.347	0.307	0.306	0.304	-
Avg stiffness @ -12°C	157	195	191	197	-
Avg m-value @ -18°C	0.287	0.264	0.258	0.258	-
Avg stiffness @ -18°C	327	363	361	383	-
Avg $\Delta T_c$ , °C	-0.5	-3.5	-3.6	-3.2	-

BBR Property	PG 64S-22 <sup>A</sup>				
	Method A	Method B	Method C	Method D	Method E
Avg m-value @ -12°C	0.318	0.305	0.293	0.302	0.299
Avg stiffness @ -12°C	103	71	82	77	79
Avg m-value @ -18°C	0.278	0.271	0.262	0.273	0.268
Avg stiffness @ -18°C	197	135	146	139	142
Avg $\Delta T_c$ , °C	-7.4	-13.1	-15.1	-14.3	-15.0

<sup>A</sup> test temperatures for Methods B, C, D, and E were -6 and -12°C

# Are agencies using $\Delta T_c$ in their specifications?

- At the time this document was developed, ten agencies in North America had or soon will adopt  $\Delta T_c$  as a specification parameter in some manner
  - There is about an even split between agencies using 20- and 40-hour PAV aging protocols
  - Most (but not all) agencies have adopted a minimum limit for  $\Delta T_c$  of  $-5.0^{\circ}\text{C}$ . The basis for that specification value is the AAPT research mentioned earlier

- $\Delta T_c$  can be easily calculated using standard BBR test data
  - Depending on lab and practices, 1-2 additional BBR tests at different temperatures may be needed
- $\Delta T_c$  appears to be an indicator of oxidative aging and loss of relaxation properties
  - Related to intermediate, durability cracking even though the tests are performed at low temperatures
  - Greater aging results in lower (more negative) values of  $\Delta T_c$

- Variability of  $\Delta T_c$  appears reasonable, as it is a product of BBR testing
  - Consider variability if establishing guidance for use
- Asphalt binders with very negative values of  $\Delta T_c$  may be more difficult to test in the BBR
  - RAS binders
- Caution when using  $\Delta T_c$  with polymer modified asphalt binders
  - Higher elastic component may make  $\Delta T_c$  more negative

# Thanks!

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